

## Linear Systems, Black Boxes, and Beyond

### Homework #1 (2012-2013), Answers

#### Q1: Fourier transforms, derivatives, and integrals

Setup is  $\hat{s}(\omega) = \int_{-\infty}^{\infty} s(t)e^{-i\omega t} dt$ , with  $s(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{s}(\omega)e^{+i\omega t} d\omega$ .

A. For  $q(t) = \frac{d}{dt}s(t)$ , find  $\hat{q}(\omega)$ .

Using the “synthesis” integral,

$$q(t) = \frac{d}{dt}s(t) = \frac{d}{dt} \left( \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{s}(\omega)e^{+i\omega t} d\omega \right) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{s}(\omega) \frac{d}{dt} (e^{+i\omega t}) d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{s}(\omega) (i\omega e^{+i\omega t}) d\omega.$$

So the coefficient of  $e^{i\omega t}$  in  $q(t) = \frac{d}{dt}s(t)$  is  $\hat{q}(\omega) = i\omega\hat{s}(\omega)$ .

B. For  $q_n(t) = \frac{d^n}{dt^n}s(t)$ , find  $\hat{q}_n(\omega)$ .

Iterating part A:  $\hat{q}_n(\omega) = i\omega\hat{q}_{n-1}(\omega)$ , so  $\hat{q}_n(\omega) = (i\omega)^n \hat{s}(\omega)$ .

C. For  $z(t) = \int_{-\infty}^t s(\tau)d\tau$ , find  $\hat{z}(\omega)$ .

Since  $s(t) = \frac{dz}{dt}$ , we can use part A:  $\hat{s}(\omega) = i\omega\hat{z}(\omega)$ , so, except possibly at  $\omega = 0$ ,  $\hat{z}(\omega) = \frac{\hat{s}(\omega)}{i\omega}$

D. Apply C to  $s(t) = \delta(t)$  to find a function whose Fourier transform, except possibly at 0, is  $\frac{1}{i\omega}$ .

Since the Fourier transform of the delta-function is 1 everywhere, the integral of the delta-function,  $h(t) = \int_{-\infty}^t \delta(\tau)d\tau$  has the required Fourier transform  $\frac{1}{i\omega}$ . Since the delta-function is an

infinitesimally narrow peak with a unit area, the integral evaluates as  $h(t) = \begin{cases} 1, t > 0 \\ 0, t < 0 \end{cases}$ . This is the

“Heaviside step function.” Its value at zero, which is formally undefined, is irrelevant for most purposes.

*Q2: Fourier transforms and moments*

Setup is  $\hat{s}(\omega) = \int_{-\infty}^{\infty} s(t)e^{-i\omega t} dt$ , with  $s(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{s}(\omega)e^{+i\omega t} d\omega$ , but now we are thinking of  $s$  as a probability distribution.

A. Write the normalization condition  $\int_{-\infty}^{\infty} s(t)dt = 1$  in terms of  $\hat{s}(\omega)$ .

Since  $e^{i\omega t} = 1$  for  $\omega = 0$ ,  $\hat{s}(0) = \int_{-\infty}^{\infty} s(t)dt$ , so the normalization condition is  $\hat{s}(0) = 1$ .

B. Write the mean (first moment)  $\langle t \rangle = \int_{-\infty}^{\infty} ts(t)dt$  in terms of  $s'(\omega) = \frac{d}{d\omega} \hat{s}(\omega)$ .

Since  $\hat{s}'(\omega) = \int_{-\infty}^{\infty} s(t) \frac{d}{d\omega} e^{-i\omega t} dt = \int_{-\infty}^{\infty} s(t)(-it)e^{-i\omega t} dt$ , it follows that  $\hat{s}'(0) = \int_{-\infty}^{\infty} s(t)(-it)dt$  and

that  $\int_{-\infty}^{\infty} ts(t)dt = i\hat{s}'(0)$ .

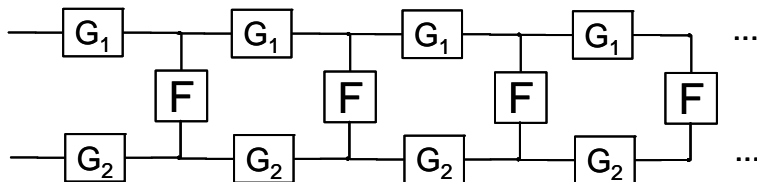
C. Write the variance (second moment)  $\langle (t - \langle t \rangle)^2 \rangle = \langle t^2 \rangle - \langle t \rangle^2 = \int_{-\infty}^{\infty} t^2 s(t)dt - \left( \int_{-\infty}^{\infty} ts(t)dt \right)^2$  in

terms of  $s'(\omega) = \frac{d}{d\omega} \hat{s}(\omega)$  and  $s''(\omega) = \frac{d^2}{d\omega^2} \hat{s}(\omega)$ .

As in part B,  $\hat{s}''(\omega) = \int_{-\infty}^{\infty} s(t) \frac{d^2}{d\omega^2} e^{-i\omega t} dt = \int_{-\infty}^{\infty} s(t)(-t^2)e^{-i\omega t} dt$ , so  $\int_{-\infty}^{\infty} t^2 s(t)dt = -\hat{s}''(0)$ .

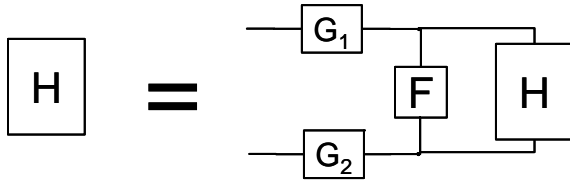
So  $\int_{-\infty}^{\infty} t^2 s(t)dt - \left( \int_{-\infty}^{\infty} ts(t)dt \right)^2 = -\hat{s}''(0) - (i\hat{s}'(0))^2 = -\hat{s}''(0) + (\hat{s}'(0))^2$ .

*Q3: The half-infinite cable (repeating indefinitely to the right)*



This is to be viewed as a network of resistors and capacitors. Calculate the impedance of the system (input applied across terminals at left) in terms of the impedances  $F(\omega)$ ,  $G_1(\omega)$ , and  $G_2(\omega)$  for  $F$ ,  $G_1$ , and  $G_2$ .

Hint: Let the composite system be  $H$ . Note the following, and then write an equation for  $H(\omega)$ .



The impedance of the composite system on the left is a series combination of three components:  $G_1$ , the parallel combination of  $F$  and  $H$ , and  $G_2$ . Therefore its impedance is

$G_1(\omega) + \frac{F(\omega)H(\omega)}{F(\omega) + H(\omega)} + G_2(\omega)$ . Since (as the hint indicates) this is equivalent to the entire half-

infinite cable,  $H(\omega) = G_1(\omega) + \frac{F(\omega)H(\omega)}{F(\omega) + H(\omega)} + G_2(\omega)$ . Solving for  $H(\omega)$  yields

$H(\omega)^2 - G(\omega)H(\omega) - G(\omega)F(\omega) = 0$ , where  $G(\omega) = G_1(\omega) + G_2(\omega)$ , or,

$$H(\omega) = \frac{G(\omega) + \sqrt{G(\omega)^2 + 4F(\omega)G(\omega)}}{2}.$$

Note concerning the continuum limit: This corresponds to allowing each subunit to represent progressively less and less length. Then  $F$  has units of impedance/cm (and increases as the segment shortens), and  $G$  has units of impedance-cm (and decreases as the segment shortens). In this limit,  $H(\omega) \approx \sqrt{F(\omega)G(\omega)}$ . This enables one to calculate the ‘‘cable length’’  $\lambda$ , which is the distance required for the transmembrane current to fall by a factor of  $e$ . To do this, note that total

transmembrane current  $I_{total}$  is  $\int_0^{\infty} e^{-x/\lambda} dx = \lambda$  times the current per unit length  $I_{peak}$  at the

injection site, but also,  $I_{total} / I_{peak}$  is inversely proportional to the total cable impedance  $H(\omega)$ ,

divided by the impedance per unit length,  $F(\omega)$ . So  $\lambda = \frac{H(\omega)}{F(\omega)} = \sqrt{\frac{G(\omega)}{F(\omega)}}$ .

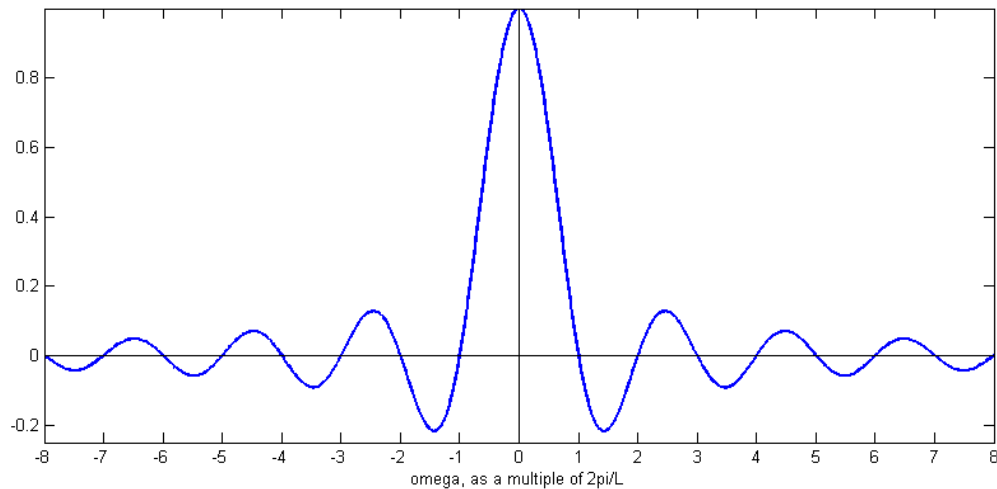
#### Q4. Boxcar smoothing

Boxcar smoothing refers to convolution with the function  $s(t)$ , where  $s(t) = \begin{cases} \frac{1}{L}, & |t| \leq L/2 \\ 0, & |t| > L/2 \end{cases}$ . Find

its Fourier transform. What does it look like? Is this a good way to smooth?

$$\hat{s}(\omega) = \int_{-\infty}^{\infty} s(t)e^{-i\omega t} dt = \frac{1}{L} \int_{-L/2}^{L/2} e^{-i\omega t} dt = \frac{1}{-i\omega L} e^{-i\omega t} \Big|_{-L/2}^{L/2} = \frac{e^{i\omega L/2} - e^{-i\omega L/2}}{i\omega L} = \frac{\sin(\omega L/2)}{(\omega L/2)}.$$

This (the “sinc” function) has a peak of 1 at  $\omega = 0$ , and descends in an envelope proportional to  $1/|\omega|$  away from zero. There are zeros at  $\omega = 2\pi k/L$ , for  $k \neq 0$ . The center lobe (at  $\omega = 0$ ) is positive, but the adjacent lobes ( $\frac{2\pi}{L} < |\omega| < \frac{4\pi}{L}$ ) are negative. So one problem with using this as a smoothing function is that it inverts the phase of non-negligible frequency components.



```
>> x=[-8:0.01:8];
>> y=sinc(pi*x);
>> plot(x,y)
>> hold on;
>> plot([-8 8],[0 0],'k')
>> plot([0 0],[-0.5 1],'k')
>> set(gca,'YLim',[-0.2 1])
>> set(gca,'YLim',[-0.25 1])
>> xlabel('omega, as a multiple of 2pi/L')
>> set(gca,'XTick',[-8:8])
```